

# **Oscilloscope Probing**

# Andrew D. Zonenberg, Ph. D

# Introduction

### **Today's class**

- Lecture followed by hands-on lab
- Stop me at any time with questions
- Bathroom / emergency procedures
- Slides are on my GitHub (CC BY-SA 4.0)
  - https://github.com/azonenberg/electronics-training/tree/master/oscilloscope-probing

# Learning goals

- Pros and cons of various probe designs
- How to select the best probe for a measurement
- How to get the most out of each probe
- Understand non-idealities of real world probes

# **Lecture outline**

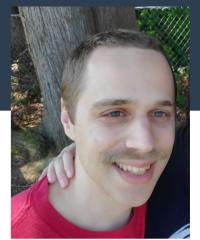
- Introduction
- What is a probe?

### • Types of probes

- R-C divider probes
- Resistive probes
- Active voltage probes
- Active differential probes
- Power rail probes
- Nearfield loop probes
- Current probes
- High voltage probes

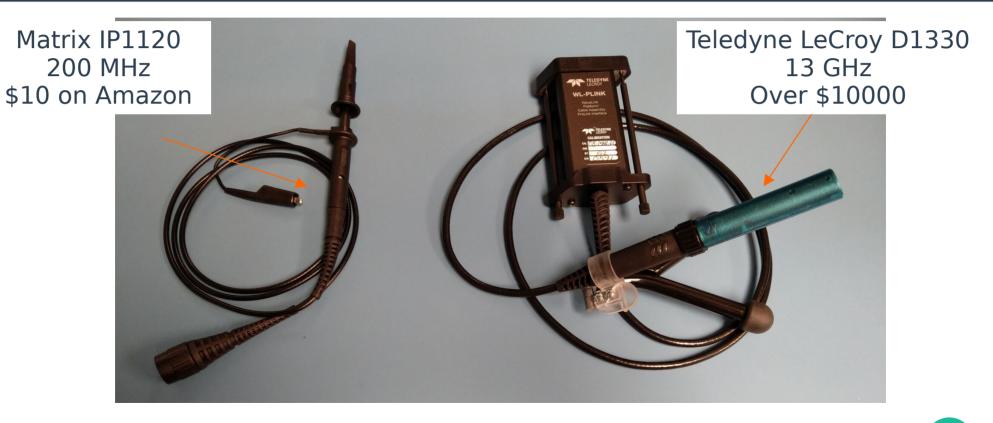
## About Me

- Ph.D Computer Science (RPI 2015)
- Embedded systems security by day



- High speed digital and test equipment by night
- Author and lead developer of glscopeclient

### Why Use One Probe Over Another?



## What is a Probe?

- Both electrical and mechanical components
- Takes signal from board and puts into instrument

# The ideal probe

- No influence on DUT behavior
- No noise
- No loss
- Low cost
- Unlimited frequency / voltage range
- Doesn't exist!
  - All real probes are compromises

# **Attributes of a probe**

- Bandwidth
- Attenuation
- Noise
- Flatness
- Loading
- Voltage range
- Linearity

- Cost
- Durability
- Ergonomics

# **Example Hardware**

### • I'm primarily a Teledyne LeCroy shop

- Most probes we'll discuss or use are made by LeCroy (or Pico)

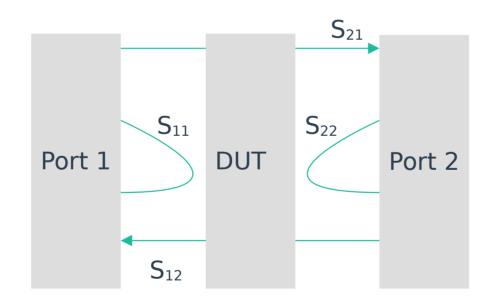
### This does not imply they're the best probes ever

- I'm just picking examples from what I have handy

### • We have a circuit with N ports

- Typical probes are 2-port networks
- RF energy is applied to one port
- Some signal comes out each port
  - Outputs / reflections have amplitude and phase shift
- Model this as a NxN "scattering matrix"

• Notation: S<sub>xy</sub> is path to X from Y



### • Each S-matrix element is a complex number

- Real and imaginary
- Or (often easier to think about) magnitude and phase angle
- Value is frequency dependent
- Nonlinear effects can create harmonics
  - S-parameters only model linear behavior
  - Keysight developed X-Parameters for modeling nonlinearities.
    This is beyond the scope of today's discussion.

### Typically measured with a VNA

- Can also simulate, etc

### • Port numbering is arbitrary

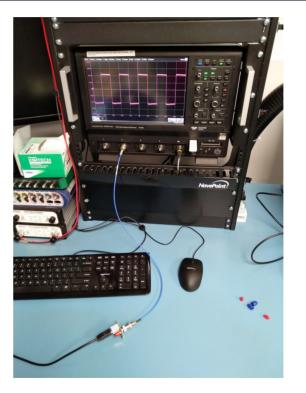
- For examples in today's class, 1 = DUT end, 2 = scope end

# **Direct Coaxial Connection**

# When Is A Probe Not A Probe?

### • When it's just a cable!





# External 50Ω Termination

- Lower end scopes lack native 50 $\Omega$  terminations
- Can use in-line or T terminations at lower freqs





# In-Line Terminator vs Native 50 $\Omega$ Input

# Reflection off stub between terminator and scope frontend

#### Matched input No reflection

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Note rise time difference:  $\checkmark$ This scope is 4 GHz BW in 50 $\Omega$  mode, 500 MHz in 1M $\Omega$  mode

# **Direct Coaxial Connection: Advantages**

### Lowest possible noise

- No external amplifiers
- No attenuation so need less frontend gain
- Low cost no expensive probe needed
- Flattest possible response
  - Only source of error is cable loss
  - Can de-embed this if cable is characterized

# **Direct Coaxial Connection: Disadvantages**

### • Requires $50\Omega$ scope input

- Inline termination works OK at lower freqs
- Reflection issues at higher speeds
- High loading on DUT
  - Probe presents a  $50\Omega$  load

### • Limited range

- Most  $50\Omega$  scope inputs are  $\pm 5V$  max range
- Many higher BW inputs are even less (±2V is common)

# **Direct Coaxial Connection: When to Use**

- If your DUT already has coaxial test points
- Measuring end of unterminated 50  $\Omega$  line
  - Empty DIMM or PCIe socket
  - Card edge connector
  - Unpopulated footprint



- Ideal reference signal to compare probe against
  - It's hard to get flatter response than a short cable

# **R-C Divider Probe**

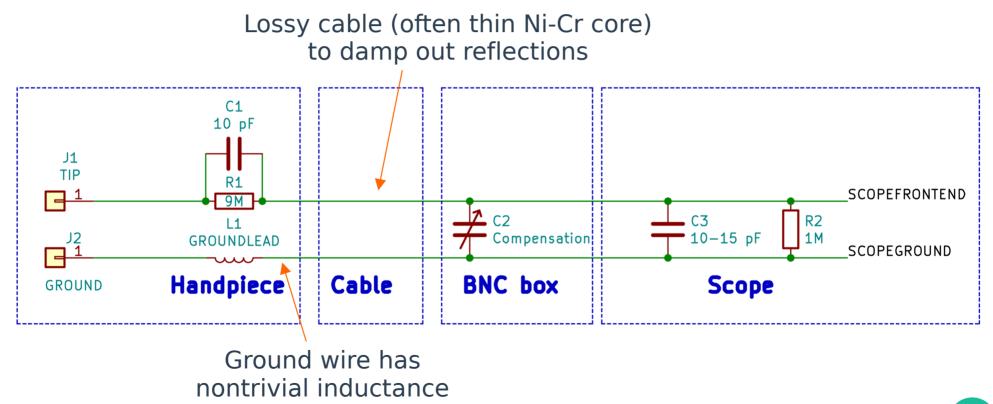
### **R-C Divider Probe**

- You've all used this one
- Dates to the vacuum tube era!





### **R-C Divider Probe**



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# **R-C Divider Probe: Compensation**

### • Trimpots / caps near BNC

- Simple design is a single C
- Higher end probes may have multiple trimmers for fine tuning

### Adjust for desired frequency response

- Usually target is broadband flatness
- For narrowband measurements, optimize for that region
- Generally not portable across scope models
  - If moving probe to another instrument, re-compensate

# **R-C Divider Probe: Compensation**



# **R-C Divider Probe: Loading**

- 10M $\Omega$  input impedance is great!
  - ...right?

# We might have forgot something :(



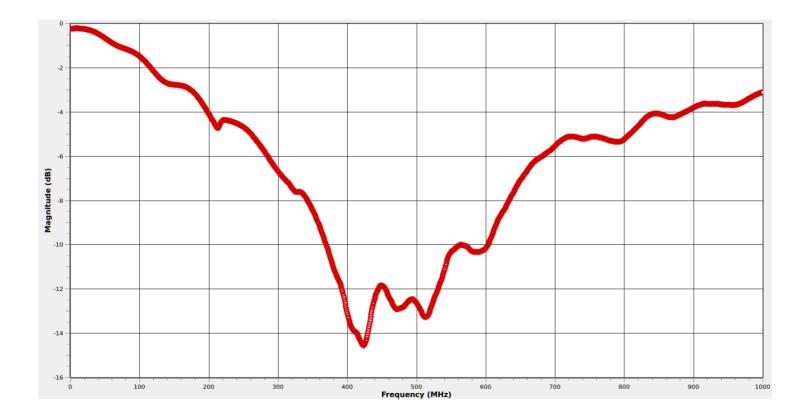
# **Probe Loading**

- Placing probe on a circuit *changes its behavior*
- This can manifest as a "heisenbug"
  - DUT stops working when you probe it, or (worse)...
  - DUT only works when you probe it!
  - New, unrelated failure introduced by probing

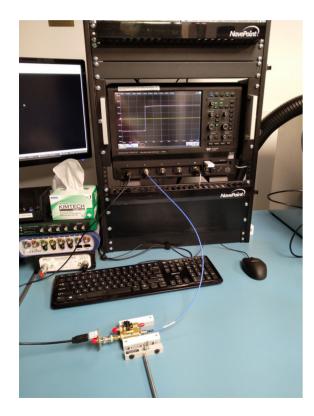
### **S**<sub>11</sub> Measurement Setup

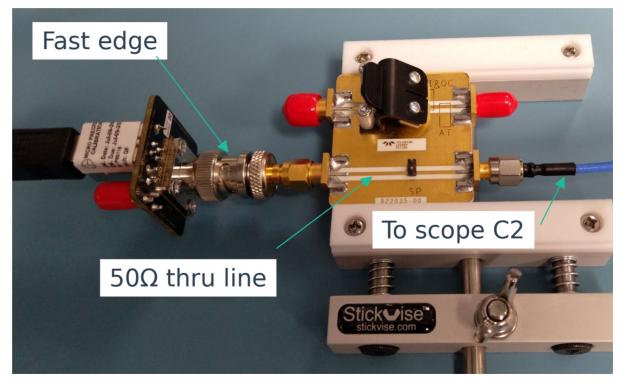
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# **R-C Divider Probe: S<sub>11</sub> (across open)**



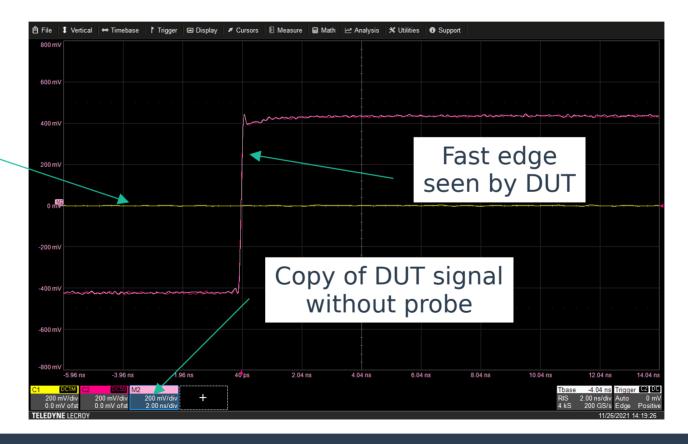
# **Time Domain Loading Measurement Setup**





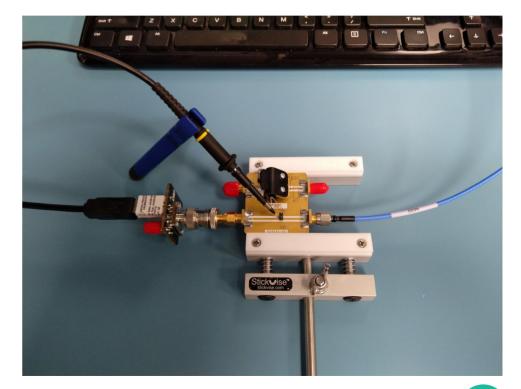
### **Baseline Measurement**

Probe is off the DUT



# Now let's add the probe...

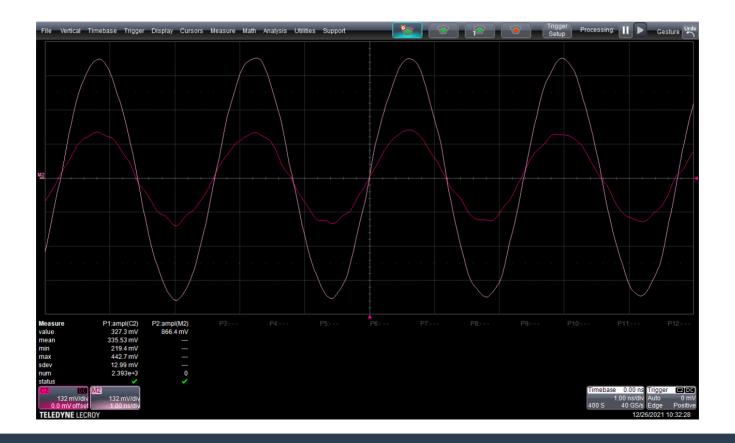
• What happens to the signal on the DUT?



### With Probe On DUT



# **Pure-Tone Loading Example (High-Z Line)**



# **R-C Divider Probe: Ground Inductance**

#### Input is very capacitive

- Any extra L will cause ringing

### Forget that alligator clip ground for anything fast

- How fast is "fast"? Let's find out...

### Generally, tradeoff of convenience vs performance

- Alligator wire: super convenient, huge L
- Z-ground: trickier to use, moderate L
- Spring: hard to use, small L

# Challenges of measuring probe S<sub>21</sub>

### • Measuring $S_{11}$ of a probe is straightforward

- Same way you'd use a VNA to measure anything else
- We don't care much about S<sub>22</sub> or S<sub>12</sub>
  - Scope doesn't drive its end of the probe
- But S<sub>21</sub> path is tricky!
  - Active probes proprietary power/signal interface
  - R-C divider probes:  $10M\Omega Z0$ , not  $50\Omega$

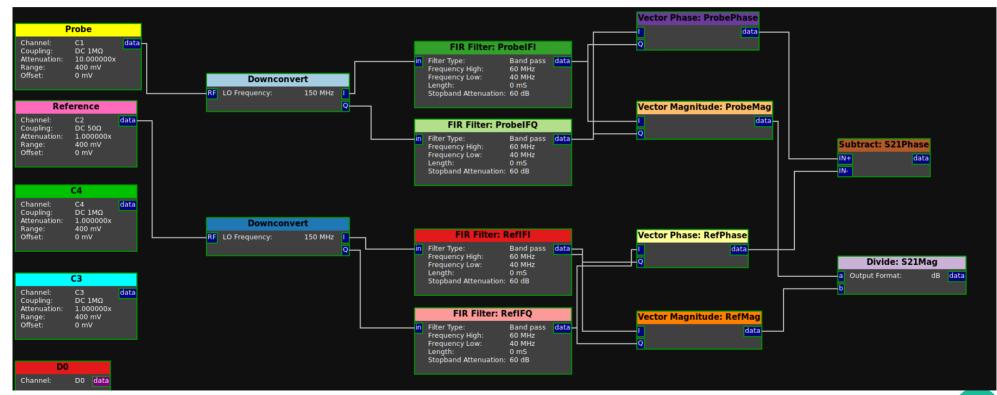


# Scope based "mixed signal VNA"

#### • Use scope as direct sampling RX for S<sub>21</sub> path!

- Port 1: Tone applied to probe tip
- Port 2: Digitized scope waveform
- Split tone to provide phase-locked reference
  - Scope CH2 = RF reference port
  - Scope CH1 = DUT port 2
- Digital downconversion of both ports
  - Then calculate ratiometric I/Q phase/amplitude

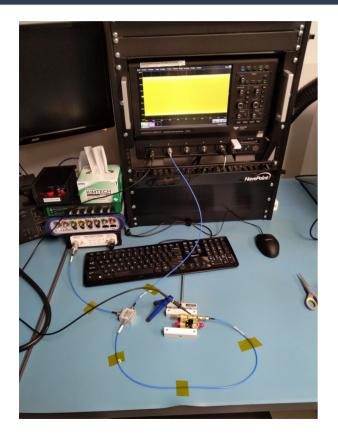
# **RX Filter Pipeline (example for 200 MHz Fin)**

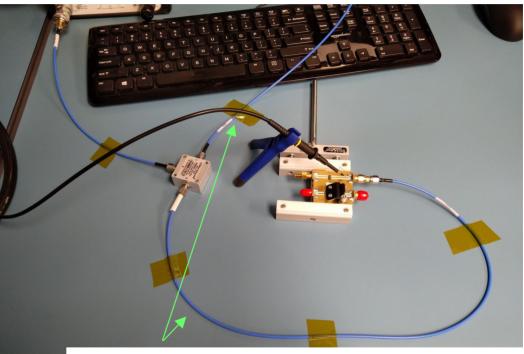


### **Raw / Processed Data**

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File Setup View Add Window Help		Opacity
	9.31 μs 9.315 μs 9.32 μs 9.325 μs 9.33 μs 9.33 μs 9.34 μs 9.34 μs 9.345 μs 9.35 μs 9.355 μs 9.36 μs 9.36 μs 9.37 μs 9.37	75 μs 9.38 μs 9.385 μs 9.39 μs 150 mV 100 mV
Probe : 2 MS 20 GS/s		100 mV 50 mV 0 mV -50 mV -50 mV -100 mV -150 mV
Reference : 2 MS 20 GS/s		148.2301 m 98.2301 m 48.2301 m 48.2301 m -1.7699 m -51.7699 m -151.7699 m
Waveform Group 2	Vetform Group 3	1.1 µs 1.1
Probein      229,7807 ml        9,7807 ml      9,7807 ml        9,7807 ml      9,7807 ml        9,7807 ml      -0,2103 ml        10,1803 ml      -0,2103 ml        20,1803 ml      -0,2103 ml        -30,2103 ml      -30,2103 ml        -30,2103 ml      -30,2899 ml        Probein      -28,2899 ml	31.9579 mV 31.4579 mV 30.4579 mV 30.4579 mV 29.9579 mV 71.4654 mV 71.2654 mV	149.0703 99.0704 49.0704 49.0704 -0.0226 -50.9296 -160.9296 -150.9297 149.0704 99.0704
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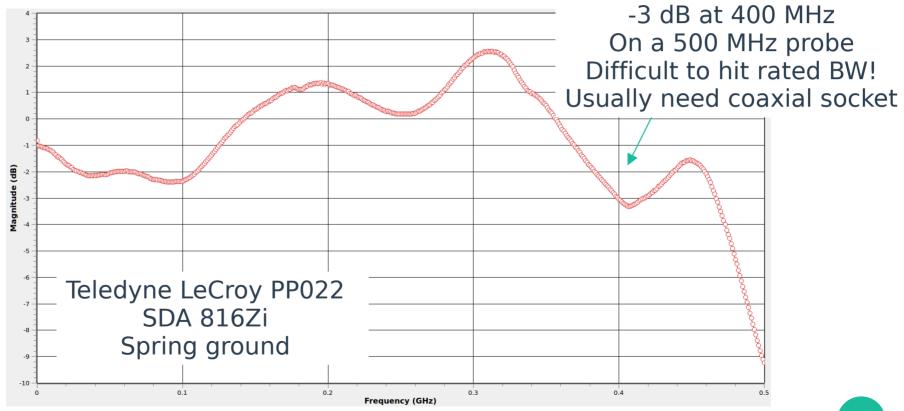
### **S<sub>21</sub> Measurement Setup**



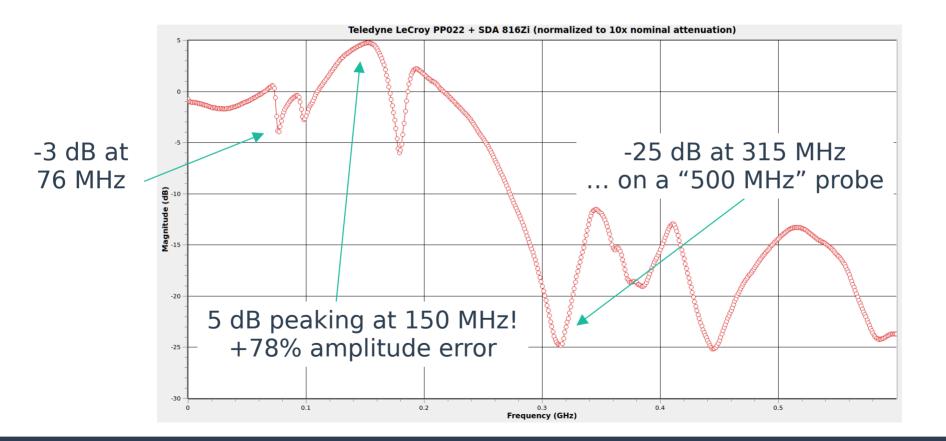


Equal length cables to scope and DUT Can calibrate out remaining skew/loss

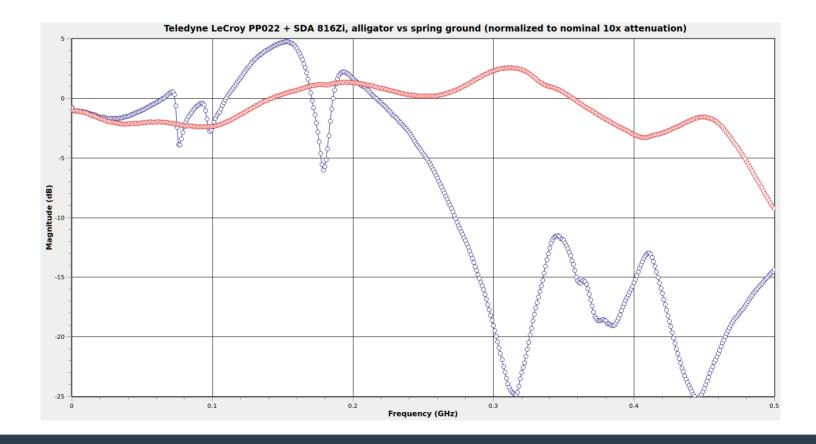
## **R-C Divider Probe: S<sub>21</sub> w/ Spring Ground**



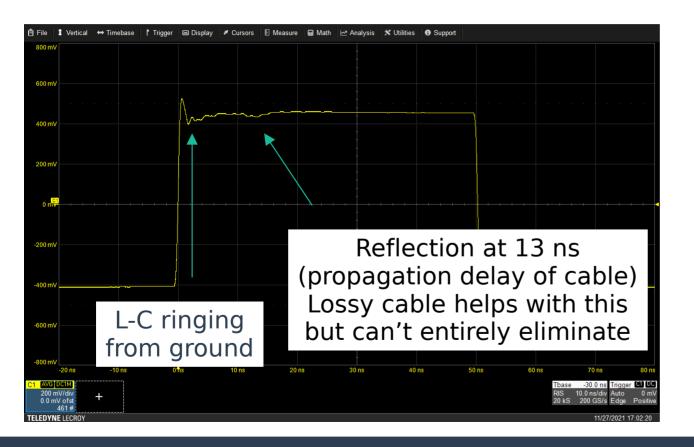
## **R-C Divider Probe: S<sub>21</sub> w/ Alligator Ground**



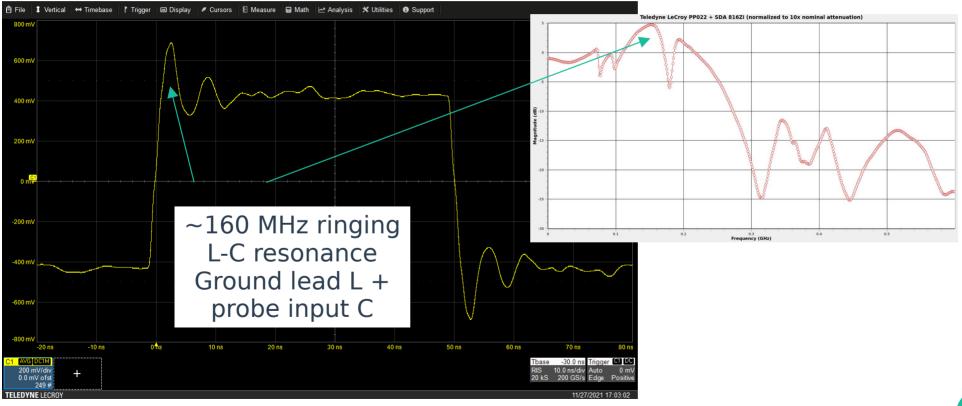
## **R-C Divider: Spring vs Alligator Ground**



## Step Response w/ Spring Ground



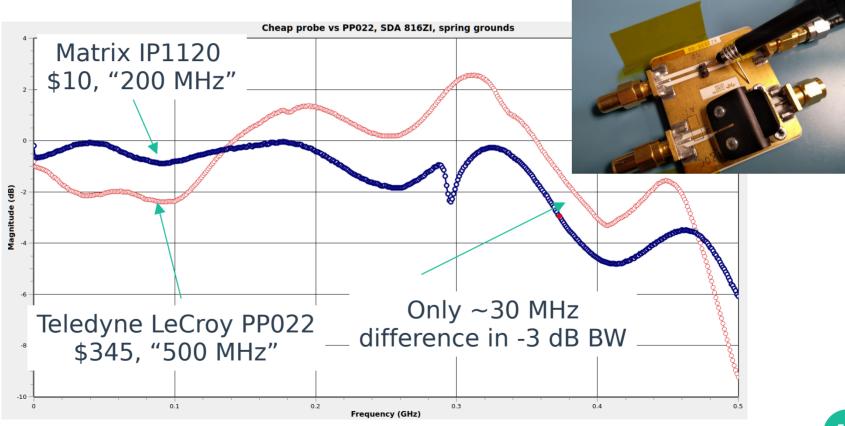
### **Step Response w/ Alligator Ground**



## **Cheap Vs Expensive Probe, Alligator Ground**



# Cheap Vs Expensive Probe, (DIY) Spring Ground



# So what did that \$335 buy you?

- Better ergonomics
- Better accessories
- More compensation adjustments
- Gain autodetection resistor
- No need to DIY a spring ground
- Worth it? Depends on your needs and budget

# **R-C Divider Probe: Strengths**

- Very low resistive loading at DC
- Low cost
  - Low 3 digits USD for a nice one
  - Cheap ones down to single digits
- Hard to damage with overload/ESD
- Generic design, no vendor lock-in

# **R-C Divider Probe: Weaknesses**

### High input capacitance

- Heavy loading on DUT
- *Extremely* sensitive to L in ground path
- Running in 1x mode makes this waaaay worse (~95 pF)!
- Requires compensation adjustment
- High attenuation (typically 10:1)
  - Not great for really weak signals
  - Worse SNR due to higher frontend gain

# **R-C Divider Probe: When to use**

### Highish voltage, low frequency analog

- (As used in vacuum tube systems!)
- Most active probes don't go past 5-10V
- Resistive probes have similar limits
- Beginners you don't trust with \$\$\$ gear
- If you have nothing better

# **Resistive Probes**

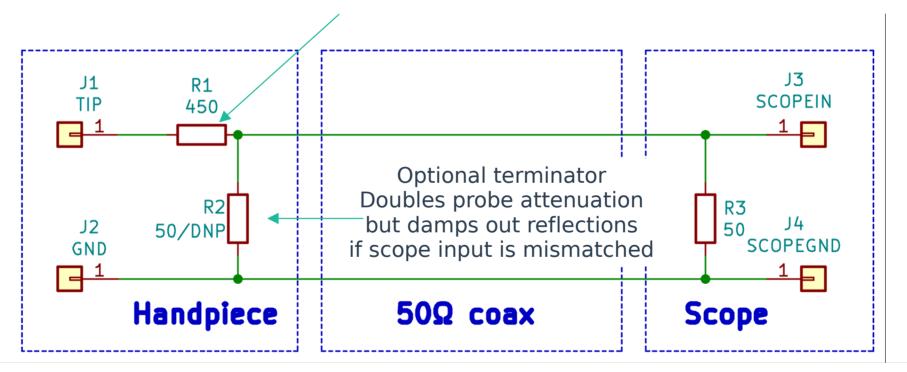
## **Resistive Probe**

### • The *other* passive probe design

- Aka Transmission line probe, Low-Z probe, Z<sub>0</sub> probe
- Conceptually super simple
  - Resistor and a piece of coax
- Doesn't get as much love as it deserves

### **Resistive Probe**

Linear tradeoff between insertion loss and loading on DUT. 450Ω for 10x, 950Ω for 20x

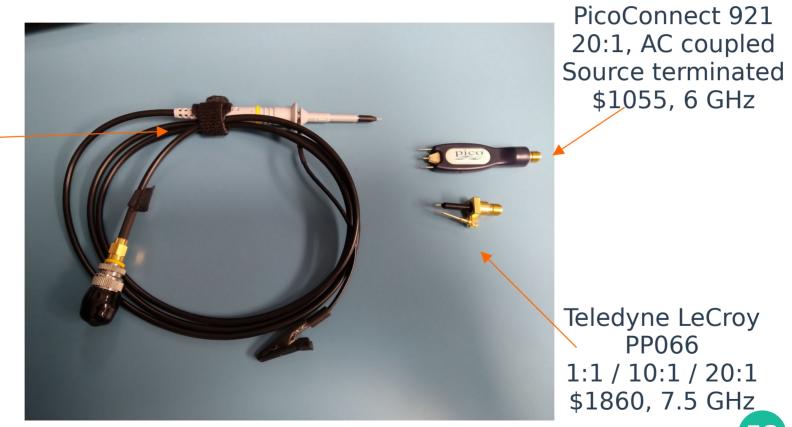


## **Resistive Probe**

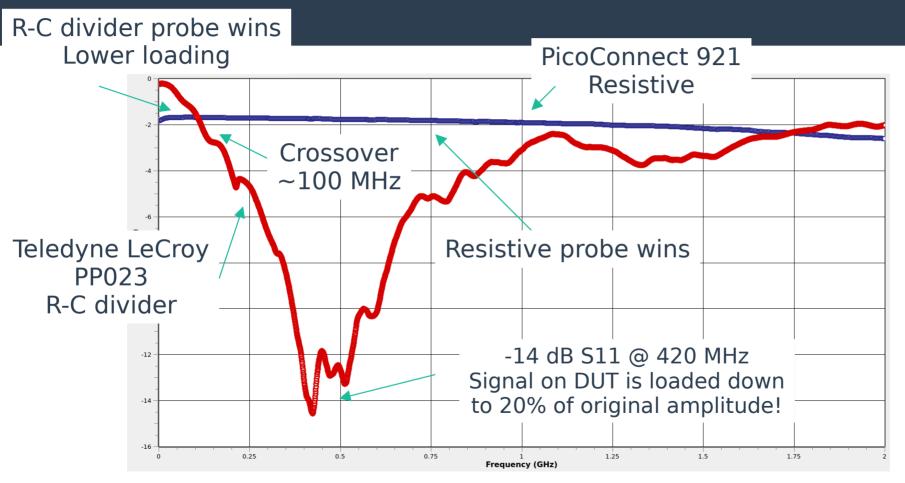
- Much higher DC loading than an R-C divider
- But response can be much flatter!
  - Ideal resistive probe has C=0 and constant  $S_{\rm 21}$  /  $S_{\rm 11}$
  - Of course, parasitics ruin our fun like always...

## **Typical Resistive Probes**

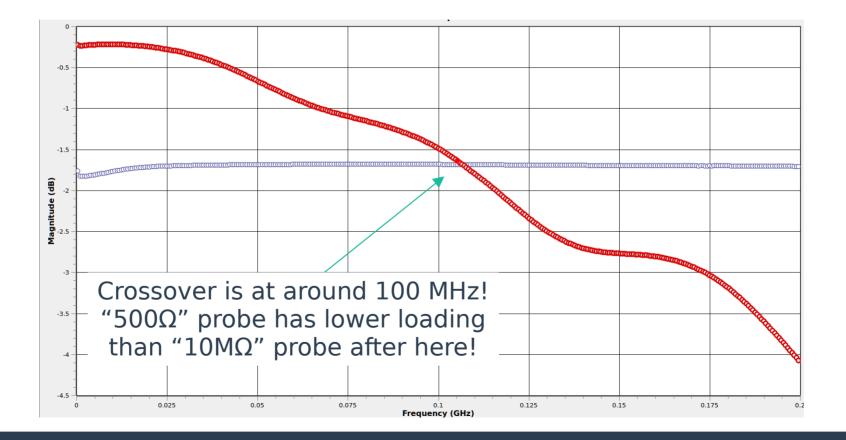
Pico TA061 10:1 \$419, 1.5 GHz



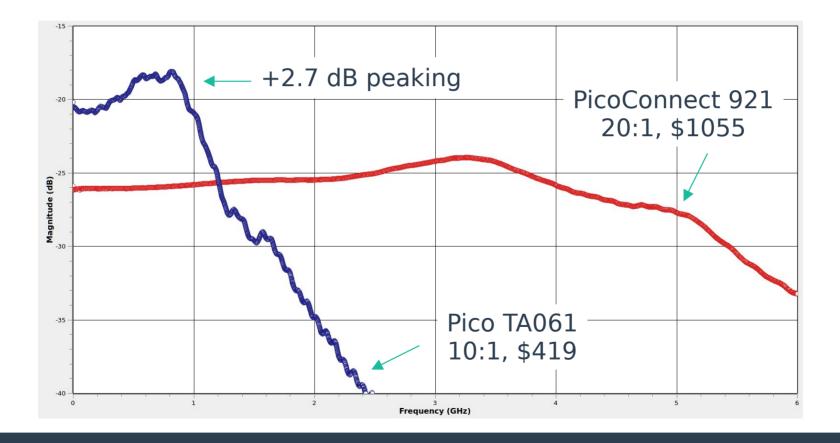
### **Resistive Probe: S11 vs R-C Divider**



### **Resistive Probe: S11 Crossover**



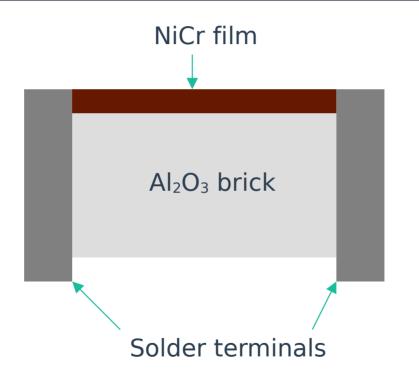
### **Resistive Probe: S<sub>21</sub> Flatness Across Models**



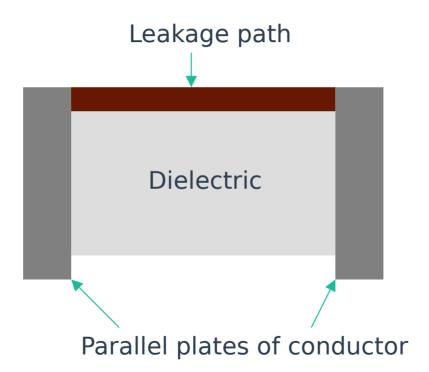
## **Resistive Probe: S<sub>21</sub> Flatness Across Models**

- Lower cost probe has much worse flatness
- But why?
- Let's look at some of the effects in play

## **Chip Resistor Cross Section**



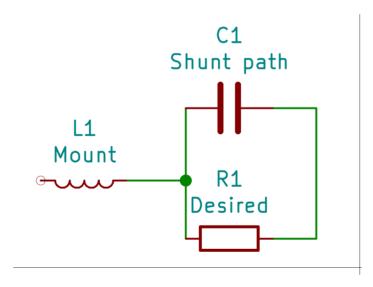
### But from a different perspective...



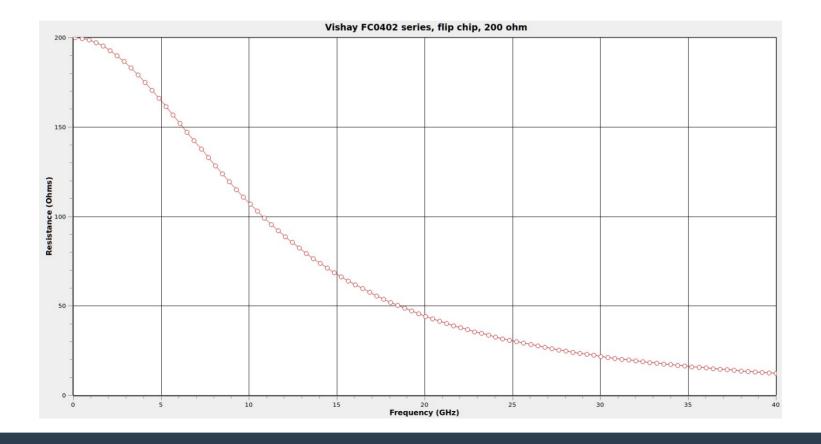


## Yep, it's a capacitor!

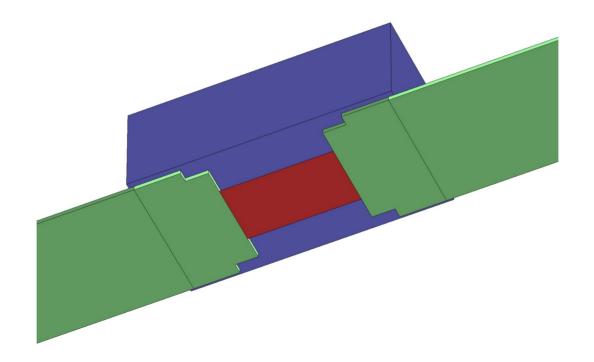
Here's a better model of a real resistor



### **Real Resistor Behavior**



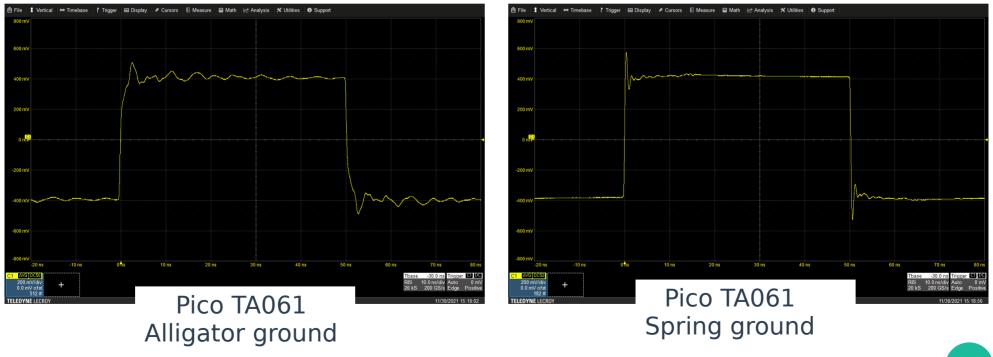
### **Flip-Chip Resistors**



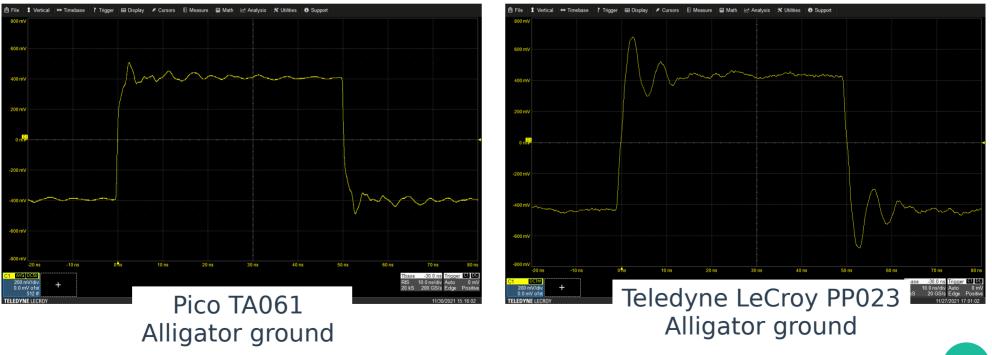
# **Resistive Probe: Ground L Sensitivity**

- Much less input C than an R-C divider
  - Low end ones (Pico TA061) can be as high as 2 pF
  - Better ones (PicoConnect) are hundreds of fF
- Less C means less ringing for same L
  - You can often get away with worse grounding vs R-C divider

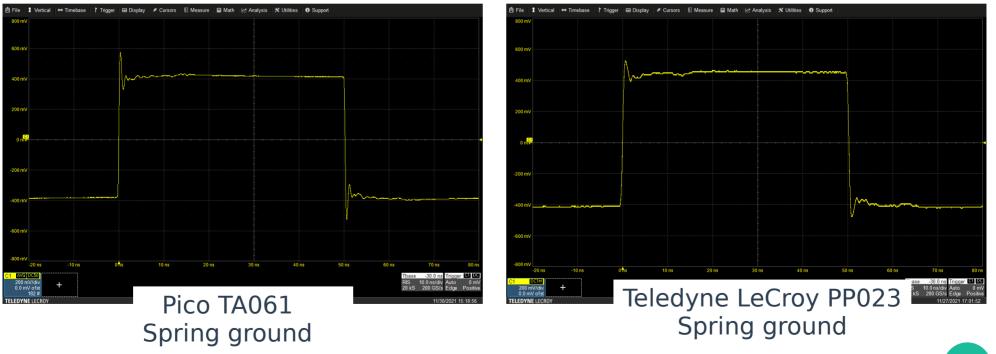
## **Resistive Probe: Ground L Sensitivity**



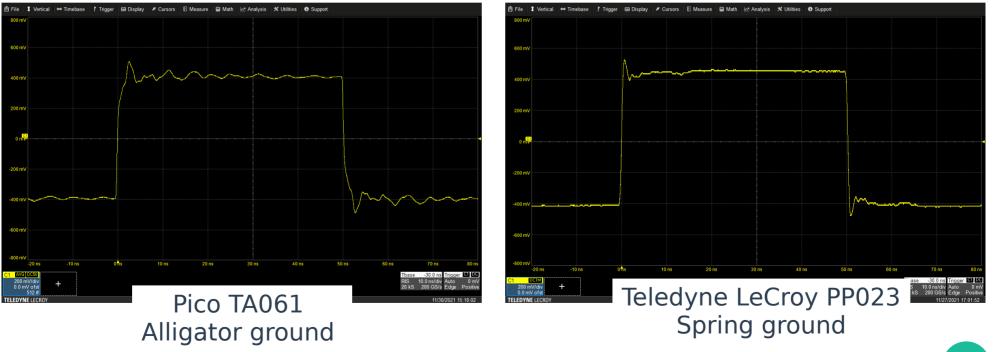
# **Resistive Probe: Ground L Sensitivity vs R-C**



# **Resistive Probe: Ground L Sensitivity vs R-C**



## **Resistive Probe: Ground L Sensitivity vs R-C**

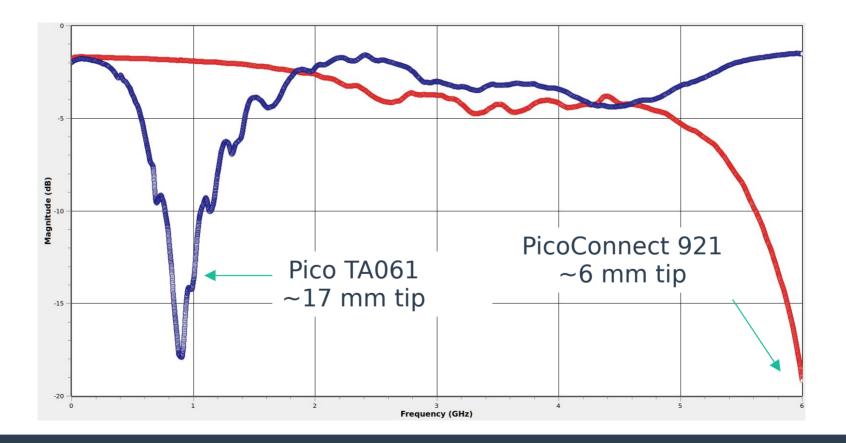


## **Resistive Probe: Input Stub**

#### Distance from probe tip to resistor is critical

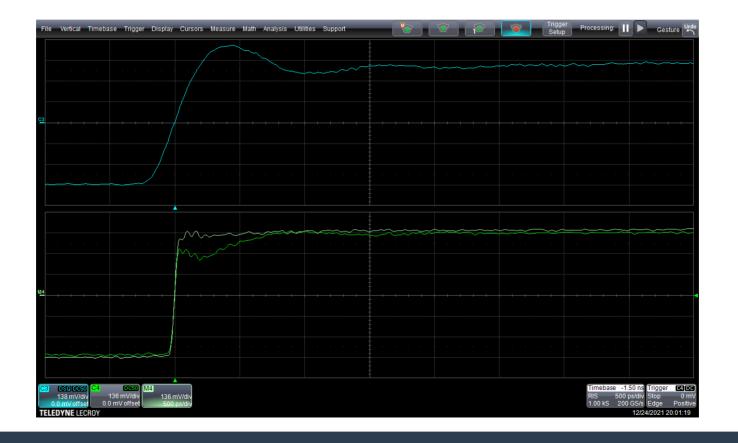
- This is an unterminated low-Z stub!
- Reflection off resistor causes 1/4 wave null in response
- Longer tip needle makes this effect worse

#### **Resistive Probe: Input S11 vs Needle Length**



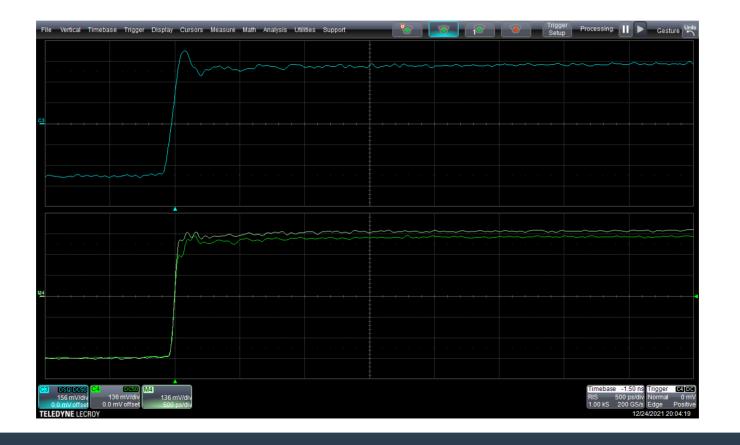
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## **Resistive Probe – Time Domain Loading (TA061)**



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## **Resistive Probe – Time Domain Loading (921)**



### **Resistive Probe – Input Stub**

#### Ideally we want no reflection at all!

- But how can we get that?
- Need to eliminate the mismatched stub somehow...

# **Resistive Probe – Reducing Reflections**

#### What if we match tip Z<sub>0</sub> to probe resistance?

- For example,  $500\Omega Z_0$  for a  $500\Omega 10:1$  probe

### This eliminates mismatch at tip-to-R junction

- All power we don't sample is instantly reflected back to DUT

# **Resistive Probe – Reducing Reflections**

#### There's just one problem...

- The impedance of free space is  $\sim 377\Omega$
- Matched tip is impossible with a 10:1 or 20:1 probe
- Doable (maybe) with a 5:1, but mechanically tricky

# **Resistive Probe – Reducing Reflections**

#### Alternative: Make the stub really short

- Move the null past the band of interest

### Lots of fun ways to do this

- Castellated probe tips
- Solder-in damping resistors
- Carbon fiber tip needles

## • Any of these sound familiar?

- We'll return to this in a later section...

# **Resistive Probe: Strengths**

- Excellent price / performance ratio
  - Nothing else gives you GHz of BW for \$1K!
  - Prices typically mid 3 to low 4 digits USD
- No active components fairly ESD resistant
- Generic design no vendor lock-in

# **Resistive Probe: Weaknesses**

#### Relatively high DC loading

- Not suitable for use on lines with pullups

#### • May disturb DC bias on DUT

- Can mitigate this w/ coaxial DC block
- Some probes include AC coupling cap

## High attenuation (typically 10:1 or 20:1)

- Can reduce attenuation at the cost of worse DC loading

## **Resistive Probe: When to Use**

#### Fast digital signals with push-pull drivers

- Excellent general purpose embedded debug probe
- Easily usable out to several Gbps
- Low impedance analog
  - Great for  $50\Omega$  RF

# High Impedance Active Probes



# **High-Z Active Probe**

- FET amplifier in probe head
- Typically fixed HW gain
  - Some (not all) provide offset capability
- High DC input resistance (M $\Omega$  range)
- Relatively low input C (usually sub-pF)

# **High-Z Active Probe**

#### Most are made by scope vendors

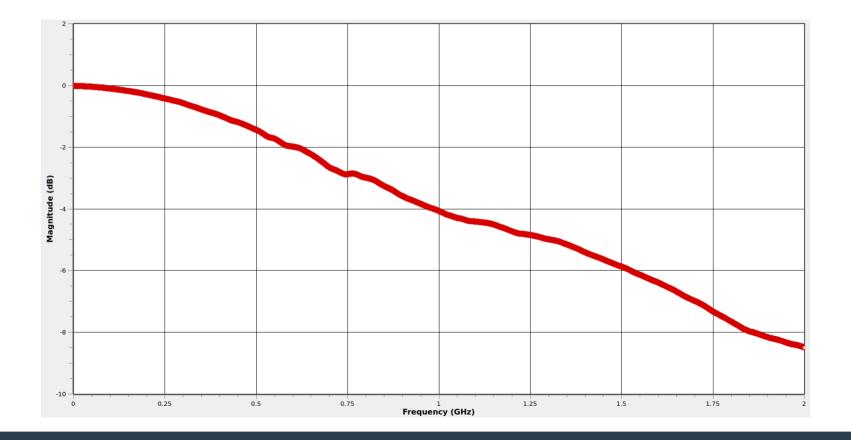
- Proprietary interface, not portable across makes
- Some third party ones exist
  - Tetris by PMK (1 to 4 GHz models)
  - External power supply,  $50\Omega$  BNC to scope

# **Teledyne LeCroy ZS1500**

- Probe head based on PMK Tetris 1500
  - 1.5 GHz, 1MΩ || 900 fF
- ProBus control pod
  - Adds ± 12V offset capability
  - (PMK version has no offset DAC)

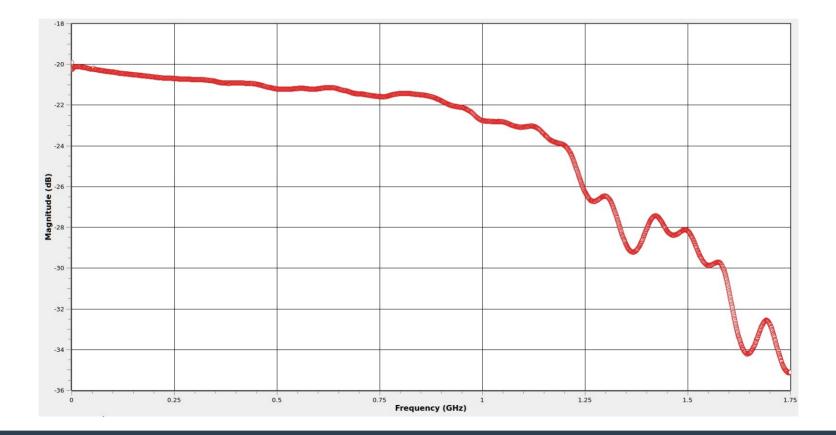


#### ZS1500 – S<sub>11</sub> w/ Leaf Ground



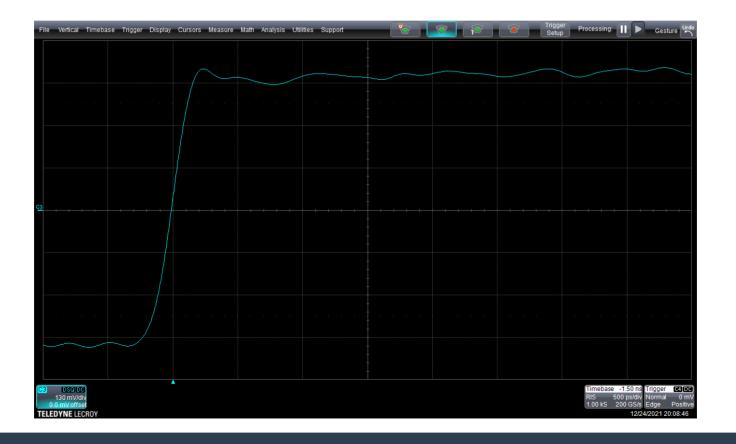
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#### ZS1500 – S<sub>21</sub> w/ Leaf Ground

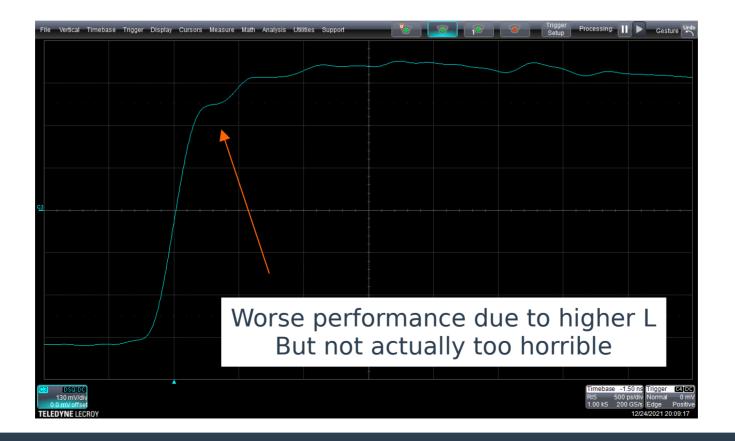


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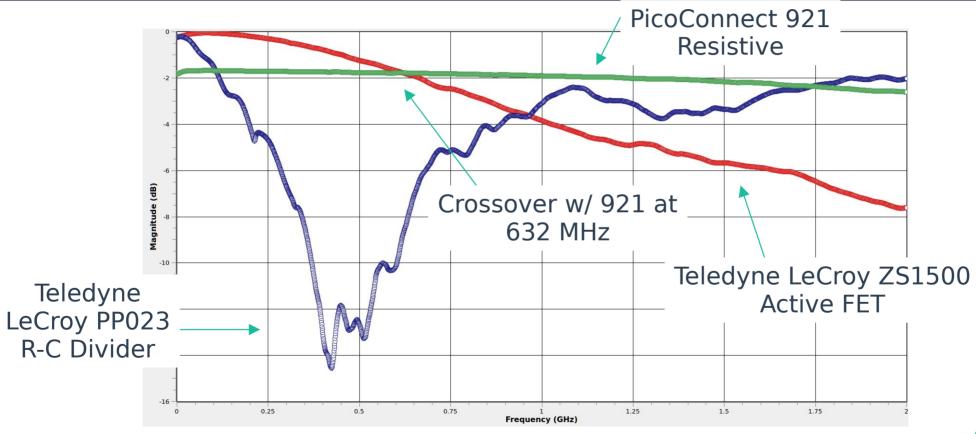
#### ZS1500 – Step Response w/ Leaf Ground



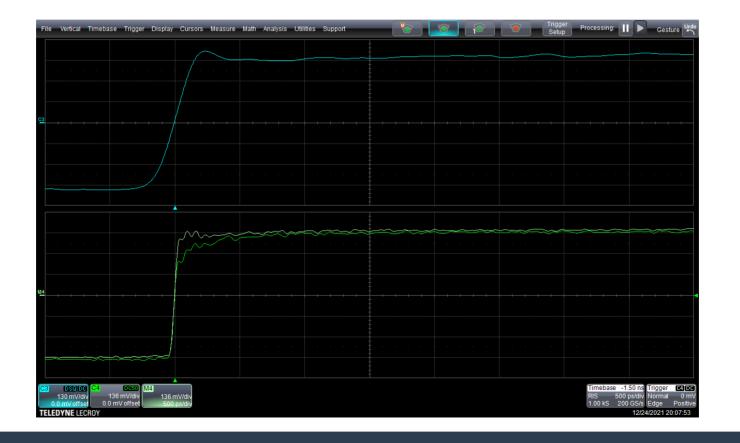
#### ZS1500: Step Response w/ 7cm Wire Ground



### ZS1500 – S11 Across Open



## ZS1500: Time Domain Loading w/ Leaf Ground



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# **High-Z Active Probe: Strengths**

- Lowest DC loading of any common probe
  - Maintains high input Z much longer than R-C divider
- Relatively low capacitance
- Somewhat tolerant of poor grounding
  - Resistive probes are usually better at this, though

# **High-Z Active Probe: Weaknesses**

- ESD sensitive
- Expensive (low-mid 4 digits USD)
- High attenuation (typically 10:1)
- Small but non-negligible input capacitance

# **High-Z Active Probe: When to use**

- Loading-sensitive low to mid speed signals
  - The ZS1500 is my probe of choice for crystal oscillators
- Excellent general purpose embedded debug probe
  - But you can buy 4+ resistive probes for cost of one FET probe!
  - Don't go out and buy a case of them unless you really need to

# **Active Differential Probes**

# **Differential Probe**

- Differential amplifier fed by probe tip
- Typically used for low swing, high BW signals
  - HV diff probes exist, will be covered separately

# **Differential Probe: Input Considerations**

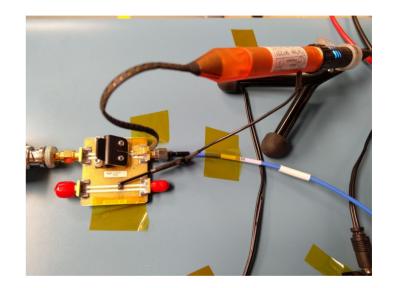
- Loading
- Common mode range
- Differential dynamic range
- Damage levels
- Overload recovery

# **Differential Probe: Grounding**

- Input signal isn't measured WRT ground, but...
- Very limited common mode range
  - $\pm$  5V for Teledyne LeCroy DH series
  - ± 2.4V for Teledyne LeCroy D400A-AT
- Board needs to share same DC ground as probe
  - No need for a low-L RF ground path!

# **Differential Probe: Grounding Methods**

- Ground from another probe
- Grounded power supply
- Ground input on amplifier
  - Only need to use one per DUT
- USB / UART / JTAG cable
- Coax shield





## **Differential Probe: Simplified Schematic**



# Loading (Teledyne LeCroy D420-A, SI tip)



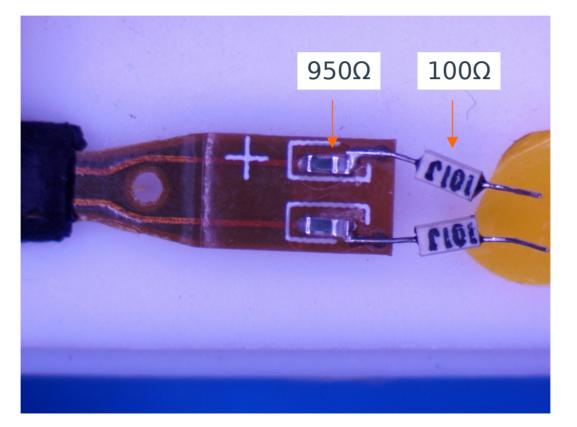


# **Differential Probe: Tips/Accessories (D1330)**



# Solder-In Tip (D1330-SI)

Tip is just two resistive probes!

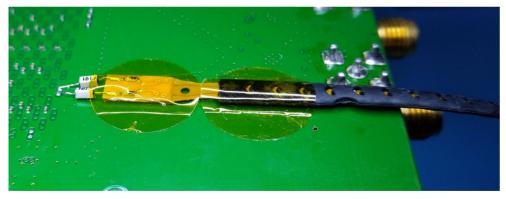




# **Differential Probe: Securing Tips**

#### • Solder-in probe tips are fragile!

- Cannot handle significant shear forces
- Secure them with tape or dedicated probe clips







# **Differential Probe: Securing Probe Body**

- Amplifier is large and heavy compared to tip
- If it moves, it will damage the tip
- Use provided holders
- Taping wires down helps too



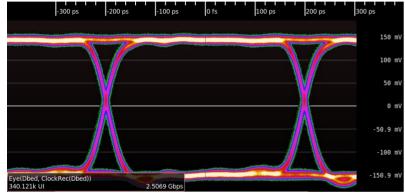


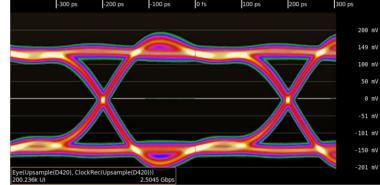
## **Overload Recovery (LeCroy D1605)**



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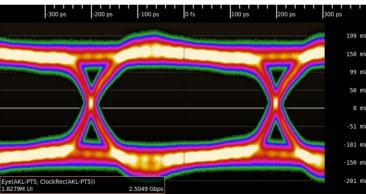
### Eye Pattern Comparison: 2.5 Gbps PRBS-9





LeCroy D420-A (Active differential) Strong overshoot Low noise

Direct coaxial input Best performance High loading



Antikernel Labs AKL-PT5 (Resistive) Slight overshoot Worse noise



### **Differential Probe: Strengths**

#### Relatively low DC loading

- Often not as low as high-Z active probe
- Very low capacitance
- Very tolerant of poor grounding
  - Ground is only used to keep common mode in range

### **Differential Probe: Strengths**

- Rejection of common mode noise
- Saves scope channels when probing a diff pair
  - Psuedo-differential input uses 2 channels + math function
- Low net attenuation (typ range /1 to /5)
  - Probe head has significant attenuation = low loading
  - Amplifier means scope sees strong signal anyway



### **Differential Probe: Weaknesses**

- Very ESD sensitive
- Extremely expensive (4-5 digits USD)
- Limited range
- Overload recovery issues

### **Differential Probe: When to use**

- High speed low-swing differential signals
- High speed low-swing single-ended signals (DDRx)
  - Need to make it differential somehow
  - Most common is to measure WRT ground
  - Can also measure WRT SSTL Vref etc

### **Active Power Rail Probes**



### **Challenges of Power Rail Measurement**

- Looking for weak ripple on large offset
- DC coupled measurements are hard
  - Most active probes can't work with 5 / 12 / 24V rails
  - Even at lower voltages, often limited offset at low V/div
- AC coupled measurements lose LF content



### **Challenges of Power Rail Measurement**

- We want low attenuation to see weak signal
- But also need low loading
  - Heavy DC load will alter DUT PSU behavior



### **Power Rail Probe: Architecture**

- Split the signal into two paths
- High(ish) impedance DC path
  - Around  $50K\Omega$  is common
  - Active amplifier with large offset range (± 24-60V)
- Capacitively coupled 50Ω AC path
  - Minimal attenuation, close to 1:1
  - Entirely passive, no additive noise



#### **Power Rail Probe: Simplified Schematic**

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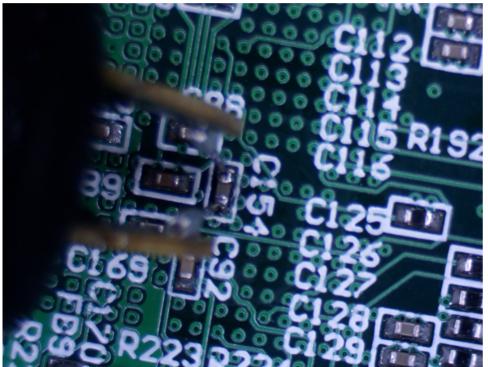
#### **Power Measurement Scenario**

- Zynq-7000 series SoC (Digilent Zybo)
- Looking at 1.0V core power rail
- Time domain and spectral analysis in glscopeclient
- Compare two 4 GHz probes on same 4 GHz scope
- Teledyne LeCroy WaveRunner 8404M-MS
  - D400-AT: 4 GHz /2.5 differential
  - RP4030: 4 GHz /1.2 power rail

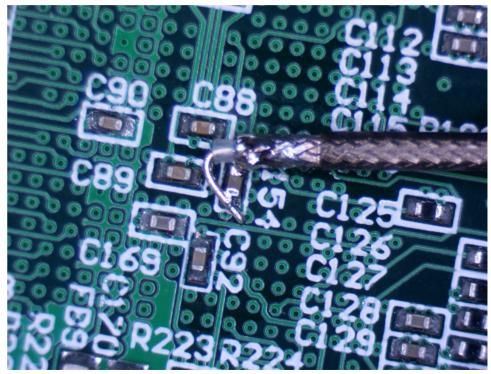


#### **Power Measurement Scenario**

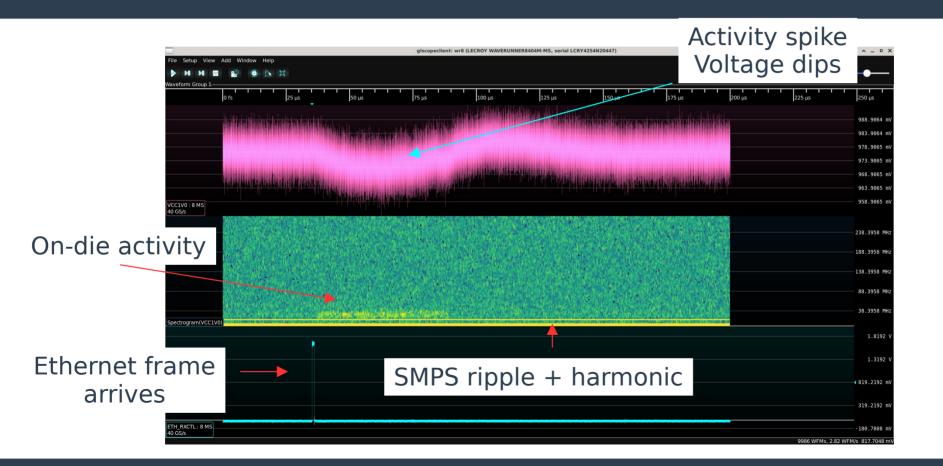
#### D400A-AT



RP4030

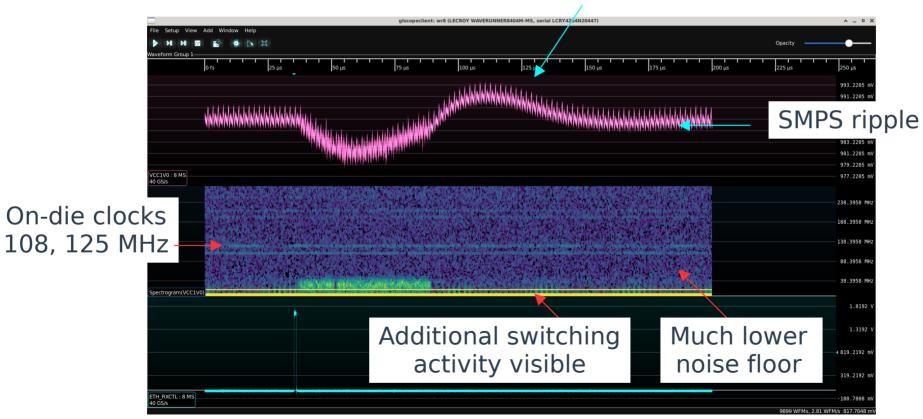


#### **Results using D400A-AT**

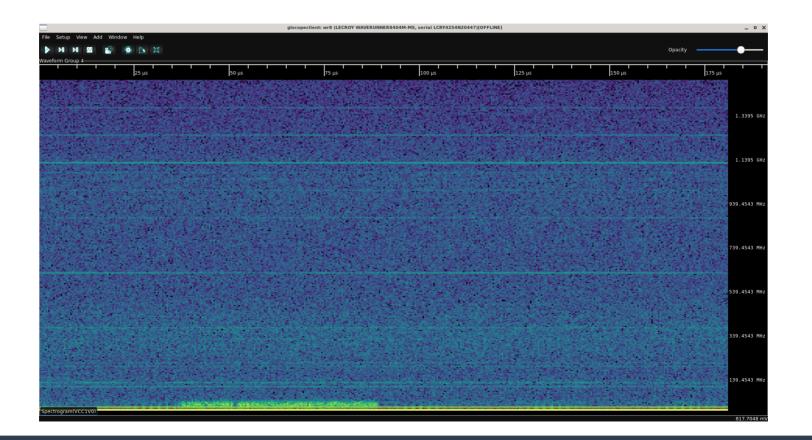


### **Results using RP4030**

# Overshoot as control loop recovers from transient



#### **Better view of spectrogram**



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#### **Power Rail Probe: Strengths**

- Extremely low noise
- Very low attenuation (close to 1:1)
  - Can detect extremely weak signals



#### **Power Rail Probe: Weaknesses**

- Expensive (RP4030 \$3016, TPR4000 \$7380)
- Limited dynamic range (± 1V or less)
- Not much good for anything but power rails

#### **Power Rail Probe: When to use**

- Power integrity measurements
- Millivolt signals on large DC bias

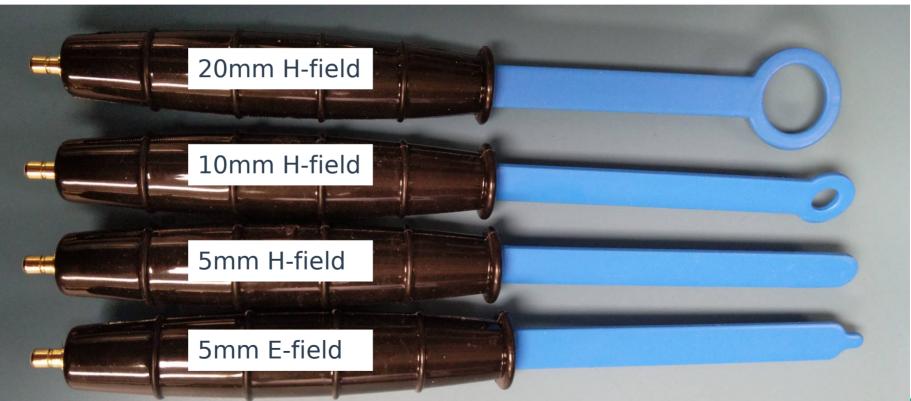


### Nearfield Loop Probes

### **Nearfield Loop Probe**

- Variants available for both H- and E-fields
- Short range RF pickup
- Typically used for EMC testing
  - Precompliance
  - Tracking down source of a failure

#### Nearfield Loop Probe (Tekbox TBPS01)



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### **Nearfield Loop Probe**

#### • Coupling varies with distance from DUT

- Not useful for quantitative intensity measurements
- But allows precise physical location of emitter to be found

#### Often used for ratiometric EMC measurements

- Place probe a fixed distance from DUT
- Compare field strength before / after some change
- Ratio doesn't scale 1:1 with far field strength
  - But usually close enough if you add some safety margin



### **Nearfield Loop Probe**

- Start with sensitive probe for long range scanning
- Move to smaller one to pin down exact source
- May need external LNA for weak signals

### **Nearfield Loop Probe: Strengths**

- Very broadband (most go to several GHz)
- Only real option for benchtop EMC testing
  - Calibrated antenna in anechoic chamber is definitive
  - But they're big and expensive!
- Allows spatial location of emitter to be found

#### **Nearfield Loop Probe: Weaknesses**

#### Very sensitive to exact position

- Not useful for quantitative measurements
- Ultra specialized
  - Not useful for much besides EMC testing



#### **Nearfield Loop Probe: When to use**

• Identifying the source of an EMC problem

### **Current Probes**



### **Current Probe: Types**

- Current transformer
- Hall effect
- Rogowski coil
- Flux gate
- Anisotropic magnetoresistive (AMR)
- Shunt resistor and differential probe



#### **AMR Positional B-Field Probe (Little Bee)**

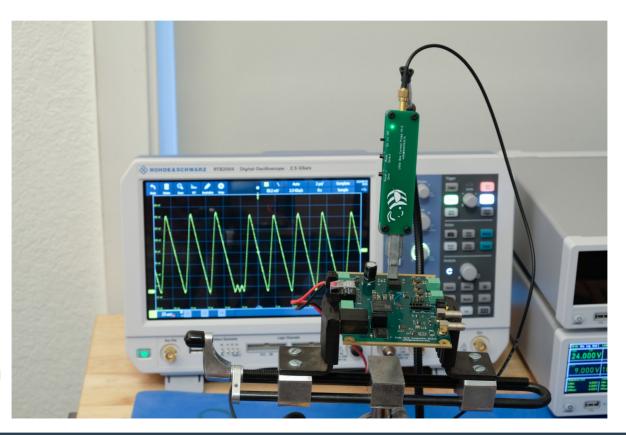


Photo courtesy of Weston Braun (Stanford)

#### **Current Probe: Strengths**

#### Doesn't require breaking circuit to add shunt

#### **Current Probe: Weaknesses**

- Some can only see AC
- Most are mechanically fragile
  - Hall sensor on ferrite core is extremely impact sensitive
- Most have to clamp around a wire
  - Difficult to measure signals on PCB
  - Provide wire loop test points if planning to measure current
- Typically designed for 10s or 100s of amps
  - Hard to measure really small currents



#### **Current Probe: When to use**

- Power supply design
- Motor control applications



## High Voltage Probes



### **High Voltage Probes**

#### Many different designs for different applications

- HV passive
- Fiber isolated
- HV differential



### **High Voltage Passive Probes**

- Classic R-C divider architecture
- Much higher attenuation
  - Teledyne LeCroy PPE5KV is 100:1, 5 kV max



### **High Voltage Fiber Isolated Probe**

- Measuring small signal on huge DC offset
  - Teledyne LeCroy HVFO108 has 35 kV common mode range
  - Amplitude ranges from  $\pm 1V$  to  $\pm 40V$
- Isolated front end driving optical fiber TOSA
- ROSA feeds scope input
- Often not a simple linear system
  - Fiber transceivers have poor linearity
  - HVFO108 uses FM over the fiber



## **High Voltage Differential Probe**

- Active differential probe for HV applications
- Pico TA044 (\$1075)
  - 70 MHz B/W
  - Switchable 100:1 / 1000:1 attenuation
  - 700 V RMS / 5 kV RMS differential range
  - 2.5 kV RMS common mode range

### **HV Probe: Strengths**

Extends range of scope to several kV



### **HV Probe: Weaknesses**

### Active probes often need batteries for remote head

- Can't be powered directly by scope
- Some fancier ones include isolated DC-DC supplies
- Passive probes have frequency derating
  - Often can't hit rated BW and voltage at once
- Low bandwidth (tens to low hundreds of MHz)



### **HV Probe: When to use**

- Measuring high voltages
- If DC isolation is required for any other reason

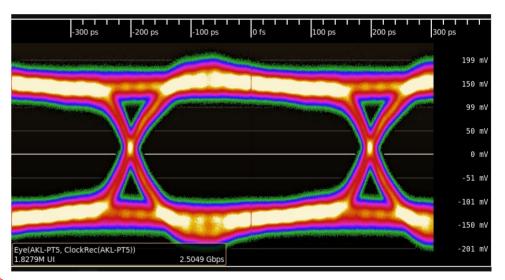


## Effects of Limited Bandwidth



### 5 GHz probe, 2.5 Gbps signal

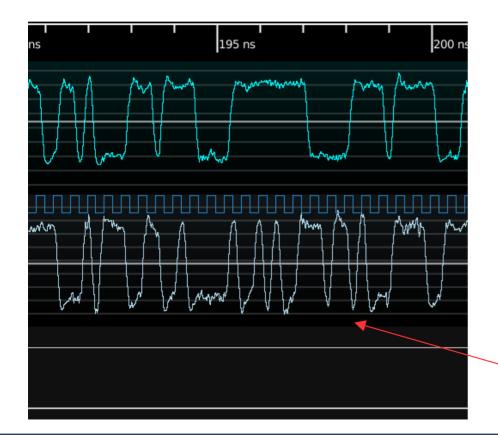


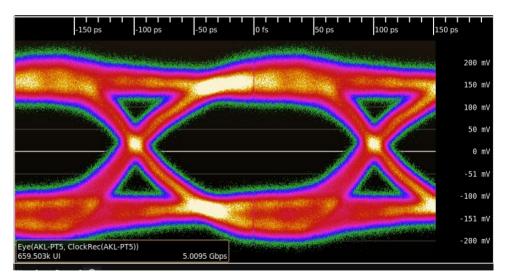


Separate rise / stable / fall regions Bits are equal amplitude

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## 5 GHz probe, 5 Gbps signal

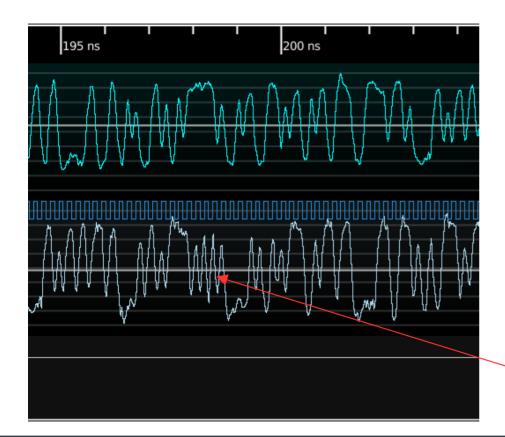


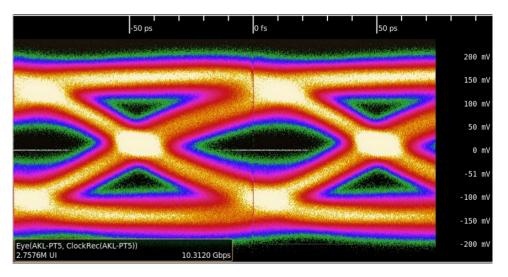


#### Bits look more sinusoidal Still roughly equal amplitude

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### 5 GHz probe, 10.3125 Gbps signal





Fast toggles do not reach full amplitude This leads to ISI



# Miscellaneous Tips

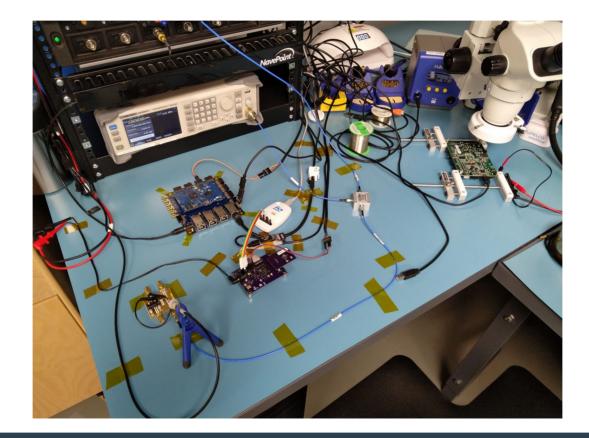


### **Passive Probe Holders**





### Securing Cabling with Kapton Tape





# **Concluding Remarks**



### Conclusions

- Huge range of options, prices, features
  - Some general purpose, some very specialized
- Easy to get garbage results with poor technique
- Understanding your probe helps you use it well

